How Stable and Active Materials would be under 100 nm

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Scheme of lecture

Transparences: <u>2-4</u> - why small scale materials ... (where)??? - why cohesion * classical macro view * under 50-100 nm ? Transparences: 5-8 - first approach (only bulk "inside" size dependency) - theory and refinement - computational example Transparences: 9-12 - second approach: concerning the surface cohesion energy - hypothesis - theory and new equations Transparences: <u>13-15</u> - computation * comparing with bulk version * comparing different metals * comparing with experimental observation Transparences: - activity - computational analysis Transparences: 17 - conclusions and overview



Why Cohesion





First Approach: bulk cohesion energy

2002, W.H.Qi, et al, [3] size dependency of cohesion energy.

$$E_{p} = E_{b} \left(1 - d_{a} \cdot \frac{1}{D_{p}} \right)$$

[J/atom of bulk] or [J/mol] (1)

The fundamental hypothesis behind Eq(1) are;

I. when a spherical particle is separated into its atoms/molecules by applying the cohesion energy, if the volume remains constant, then we may write:

$$n=d_a^3/D_p^3$$

II. by defining the surface area change during applying the given energy for separation of a particle into n atoms which apparently equals to surface energy of solid materials multiplying by the total surface area, then we may write:

$$E_n = \Delta A \cdot \delta^o$$

III. cohesion energy per atoms from the previous two points will be:

$$E = \pi \cdot \delta^{o} \cdot d_{a}^{2} \cdot (1 - d_{a} / D_{p})$$

iv. these two energies (ii. and iii.) phenomenologically are equal, then we can write:

$$E_n = E$$

Packing factor correction

in [3], regarding the steps i. condition of constant volume real materials volume packing factor

 $f_v \cdot V_p = n \cdot V_a$

$$E_{p} = E_{b} \cdot \left(1 + \frac{1}{f_{v}} + d_{a} \cdot \frac{1}{D_{p}} \right)$$

[J/atom of bulk] or [J/mol] (2)

Comparing Eq(1) and Eq(2), usual metallic crystal structure with fcc packing factor of 0.74 we expect 35% faster size variation effect respectively





Comparison of coefficient of bulk cohesion energy for Al metal.



Comparison of different cohesion energies for Al metal.





Xie, Qi: 2004 [4] from embedded NP in matrix got the wholly free standing coefficient as 3/4 in Eq(1) and said it is the surface effect

Second Approach: considering the surface cohesion energy



Schematics of surface and Gibbs free energy related things.

total Gibbs free energy of a system

$$G^{\Sigma} = n \cdot G_b + \delta \cdot A \qquad [J] \qquad (3)$$

By considering the amount of materials gathered in surface as well as bulk

$$n = n_b + n_s \quad \xrightarrow{\text{for sphere}} \quad n_s = \frac{A}{W} = \frac{\pi \cdot D_p^2}{W} \text{ and } n = \frac{m}{M} = \frac{\rho \cdot V}{M} = \frac{\rho \cdot \pi \cdot D_p^3}{6 \cdot M}$$
(4)

Consequently through Eq(3), we can write similar algorithms for any physicochemical quantity of materials like cohesion energy

$$E = n_b \cdot E_b + n_s \cdot E_s \xrightarrow{\text{then}} E_p = n_i \cdot E_i + n_s \cdot E_s \qquad [J] \qquad (5)$$

modeling the surface cohesion energy





Schematics of surface energies at outer layers

As here we assume mono atomic/molecular surface layer. then we can summarize such estimation, as:

$$E_{s} = \frac{1}{6} \cdot E_{i} + E_{s}^{2D} \xrightarrow{\text{then in } Eq(2)} E_{p} = n_{i} \cdot E_{i} + n_{s} \cdot \left(\frac{1}{6} \cdot E_{i} + E_{s}^{2D}\right) \quad \text{[J/mol]} \quad \text{(6)}$$



2D term of surface cohesion energy E_s^{2D}



Schematics of cohesion energies and surface monolayer

(7)

- suppose there is a virtual 2D monolayer surface - an amount of energy equal to E_{2}^{2D} in order to separate it into atoms/molecules

use the algorithm similar bulk (inside)

- the energy required to separate the atoms from the first layer (the one needed for compensating the 2D stability) <u>proportional</u> to making the surface area changed from initial state to areas of total separated atoms/molecules building the monolayer surface

- the proportionality factor is the surface energy of solid material, thus:

$$E_s^{2D} = \delta \cdot \Delta A_s^{2D} = \delta \cdot (A_s^{\text{final}} - A_s^{\text{initial}})$$



During the separation: assumption of constant volume rule

$$n_{s} \cdot \frac{4}{3} \cdot \pi \left(\frac{d_{a}}{2}\right)^{3} \equiv f_{s} \cdot V_{s}^{2D}$$
⁽⁸⁾

 $f_s \leq f_V$

Regarding the Fig.1. and x from volume constant condition we get:

$$n_{s} = \frac{f_{s} \cdot (10 \cdot x \cdot D_{p}^{2} - 12 \cdot x^{2} \cdot D_{p} + 8 \cdot x^{3})}{d_{a}^{3}}$$
(9)

Then Eq(7) changes to:

$$E_s^{2D} = \delta \cdot \left(n_s \cdot \pi \cdot d_a^2 - \pi \cdot D_p^2 \right)$$
 [J] (10)

By combining the hypothesis of Eqs(1-2) above, we may write further:

$$E_{s}^{2D} = E_{b} \cdot \left(1 - \frac{1}{f_{s}} \cdot d_{a} \cdot \frac{D_{p}^{2}}{(10 \cdot x \cdot D_{p}^{2} - 12 \cdot x^{2} \cdot D_{p} + 8 \cdot x^{3})} \right)$$

[J/atom surface] (11)

Combining the Eq(11) and Eq(6) regarding Eq(5), the total surface cohesion energy for complete sphere will be in [J/atom surface]

$$E_{s} = E_{b} \cdot \left(\frac{7}{6} - \frac{1}{f_{v}} \cdot d_{a} \cdot \frac{1}{D_{p}} \cdot \left(1 - \frac{f_{v}}{f_{s}} \cdot \frac{D_{p}^{3}}{(10 \cdot x \cdot D_{p}^{2} - 12 \cdot x^{2} \cdot D_{p} + 8 \cdot x^{3})} \right) \right)$$



(12)

Computation Analysis

What we have till now:

$$E_p = E_b \cdot \left(1 - d_a \cdot \frac{1}{D_p} \right)$$

original not corrected [J/atom of bulk] or [J/mol] [3] (1)

$$E_p = E_b \cdot \left(1 - \frac{1}{f_v} \cdot d_a \cdot \frac{1}{D_p} \right)$$

[J/atom of bulk] or [J/mol] (2) original corrected

$$E_{p} = n_{i} \cdot E_{i} + n_{s} \cdot E_{s} \qquad [J] \quad (5) \qquad \text{new} \qquad [J/atom surface] (12)$$

$$E_{s} = E_{b} \cdot \left(\frac{7}{6} - \frac{1}{f_{v}} \cdot d_{a} \cdot \frac{1}{D_{p}} \cdot \left(1 - \frac{f_{v}}{f_{s}} \cdot \frac{D_{p}^{-3}}{(10 \cdot x \cdot D_{p}^{2} - 12 \cdot x^{2} \cdot D_{p} + 8 \cdot x^{3})}\right)\right)$$

Xie, Qi: 2004 [4] from embedded NP in matrix got the wholly free standing coefficient as 3/4 in Eq(1) and said it is the surface effect

for AI, Ag, Ga and W





Comparison of coefficient of different cohesion energies for AI metal





Comparing the coefficient of cohesion energies for different metals



Comparing the calculated and experimental observation of cohesion energies for W metal

Conclusions and Overview - new scale of properties of nano-materials (via Cohesion scale)

i. introduction of bulk (inside) cohesion energy of nano-materials
ii. development of a thermodynamical model for surface cohesion energy of nanomaterials,
iii. series of computational analysis for comparing the materials like: Al, Ga, W and Ag metals,
iv. discussion the critical size and its relation to surface cohesion energy domination,
v. comparison the experimental values of W metal with computational simulation,

- activity of nano-particles ... (under construction)

Further Steps

-shape effect on cohesion phenomena -globalizing the activity of particles and experimental comparison (if any) -size and shape effect of first order phase transitions -size and shape effect on higher order phase transitions ? ...

-mixing or solving the particles together or in a bigger system -phase diagram (state equation) of mono-particle -state equation of multi- particles



Nomenclature

E, G: respectively cohesion and Gibbs free energy [kJ/mol] or [kJ],

f : packing factor,

 d_a, D_p : respectively diameter of atom and diameter of particle [nm],

n: number of mole [mol],

A: area of material [m²],

 δ° : surface energy per unit area at 0 K [J/m²],

 $\Delta\colon$ symbol showing the difference between two states of a quantity,

 b, i, p, s, Σ, v : in subscribe and superscript respectively: bulk, inside, particle, surface, total and volume, w, ρ, V, M, m, x : respectively molar surface area [m²/mol], density [g/m³], volume [m³], molar mass [g/mol], mass [g] and actual atomic height of mono surface layer [nm]

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